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## ON VARIOUS DYNAMIC COMPENSATIONS

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The aim of this modest note is to show that certain compensation schemes frequently used in control theory, namely regular output feedback, combined dynamic compensation, and dynamic precompensation, are input-output equivalent.

### 1. INTRODUCTION

Let  $R^{p \times q}$  and  $R^{p \times q}\{w\}$  be respectively the sets of scalar and proper rational  $p \times q$  matrices in one indeterminate  $w$  over the real field  $R$ . The units of the rings  $R^{n \times n}$  and  $R^{n \times n}\{w\}$  are respectively the non-singular and bi-proper matrices. Let us recall that an  $H(w)$  is a unit of  $R^{n \times n}\{w\}$  if and only if  $H(0)$  is a unit of  $R^{n \times n}$ . That is to say, a rational matrix is bi-proper if it is proper together with its inverse. As usual,  $I$  will denote the identity matrix.

Consider a system  $\Sigma$

$$(1) \quad \begin{aligned} \dot{x} &= Ax + Bu \\ y &= Cx + Du \end{aligned}$$

described by the quadruple of matrices  $A \in R^{n \times n}$ ,  $B \in R^{n \times q}$ ,  $C \in R^{p \times n}$  and  $D \in R^{p \times q}$  which gives rise to the transfer matrix

$$T(w) = D + wC(I - wA)^{-1}B \in R^{p \times q}\{w\}.$$

Thus  $w$  is the inverse differential operator.

Further let

$$(2) \quad \dot{x}_d = u_d$$

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be a dynamic extension of  $\Sigma$ , a bunch of  $n_d$  integrators, and let  $v$  denote a command signal, say  $r$ -dimensional one.

Consider the problem of modifying  $T(w)$  by means of a control law. The following three control laws are frequently used in the literature.

### 1. Regular Output Feedback

$$(3) \quad \begin{bmatrix} u \\ u_d \end{bmatrix} = F \begin{bmatrix} y \\ x_d \end{bmatrix} + Gv$$

$$(4) \quad \begin{cases} F = \begin{bmatrix} F_{11} & F_{12} \\ F_{21} & F_{22} \end{bmatrix} \in R^{(q+n_d) \times (p+n_d)} \\ G = \begin{bmatrix} G_1 \\ G_2 \end{bmatrix} \in R^{(q+n_d) \times r} \end{cases}$$

and

$$(5) \quad I - F_{11}D = \text{unit of } R^{q \times q}.$$

This static control law acting on the extended system (1)–(2) is often used to study the dynamic output feedback for the original system (1), see e.g. Wonham [4]. The regularity condition (5) was introduced by Descusse and Malabre [1] in order to prevent the derivatives of  $v$  to appear in  $x$ . The class of control laws (3) satisfying (4)–(5) will be denoted by  $C_1(\Sigma)$ .

### 2. Combined Dynamic Compensation

$$(6) \quad u = P(w)y + Q(w)v$$

where

$$(7) \quad P(w) \in R^{q \times p}\{w\}, \quad Q(w) \in R^{q \times r}(w)$$

and

$$(8) \quad I - P(w)T(w) = \text{unit of } R^{q \times q}\{w\}.$$

This is a general compensation scheme which makes explicit the presence of a feed-forward and a feedback in the control law. It has been found useful in the polynomial equation approach, see e.g. Kučera [2]. In most cases, the regularity condition (8) is tacitly assumed. The class of control laws (6) satisfying (7)–(8) will be denoted by  $C_2(\Sigma)$ .

### 3. Dynamic Precompensation

$$(9) \quad u = K(w)v$$

where

$$(10) \quad K(w) \in R^{q \times r}\{w\}.$$

This is a standard way of introducing a compensator when the transfer-function approach is adopted. The scheme is flexible and can be used to represent a combined compensation or a dynamic feedback alone, see e.g. Wolovich [3]. The class of control laws (9) which satisfy (10) will be denoted by  $\mathcal{C}_3(\mathcal{Z})$ .

We shall say that two classes are *input-output equivalent* if, for any control law of one class, we can find a control law in the other class such that their application to a given system will result in overall systems having the same transfer matrices.

This kind of equivalence reflects just the ability of two control laws to produce the same input-output behaviour. In particular, this equivalence says nothing about dynamical order, stability, sensitivity or other properties of control systems which depend on a particular realization. Nevertheless, this concept is useful when various feedforward/feedback configurations are studied from the input-output point of view. This is the case, for example, when solving the disturbance rejection, exact model matching or model following problems in dynamical systems.

## 2. RESULT

The aim of this note is to show that the three control laws are input-output equivalent. This would not be surprising if the control laws were unrestricted by (5), (8) and (10). What is less obvious is that the *regularity* condition (5) or (8) is equivalent to the *properness* condition (10).

**Claim.** The classes  $\mathcal{C}_1(\mathcal{Z})$ ,  $\mathcal{C}_2(\mathcal{Z})$  and  $\mathcal{C}_3(\mathcal{Z})$  are input-output equivalent.

*Proof.* The easiest way is to establish the chain of implications

$$\mathcal{C}_1(\mathcal{Z}) \Rightarrow \mathcal{C}_2(\mathcal{Z}) \Rightarrow \mathcal{C}_3(\mathcal{Z}) \Rightarrow \mathcal{C}_1(\mathcal{Z}).$$

a) To show that each element of  $\mathcal{C}_1(\mathcal{Z})$  can be realized as an element of  $\mathcal{C}_2(\mathcal{Z})$ , consider a control law defined by (3)–(5). Using (1)–(3), calculate the transfer matrices from  $y$  and  $v$  to  $u$ . On identifying with (6), we obtain

$$(11) \quad \begin{aligned} P(w) &= F_{11} + wF_{12}(I - wF_{22})^{-1}F_{21} \\ Q(w) &= G_1 + wF_{12}(I - wF_{22})^{-1}G_2. \end{aligned}$$

Since  $I - wF_{22}$  is bi-proper, both  $P(w)$  and  $Q(w)$  are proper. Moreover

$$I - P(0)T(0) = I - F_{11}D$$

is non-singular whence (8) holds. The control law (11) thus belongs to  $\mathcal{C}_2(\mathcal{Z})$ .

b) To show that each element of  $\mathcal{C}_2(\mathcal{Z})$  can be realized as an element of  $\mathcal{C}_3(\mathcal{Z})$ , consider a control law defined by (6)–(8). Calculate the transfer matrix from  $v$  to  $u$  and compare it with (9) to obtain

$$(12) \quad K(w) = [I - P(w)T(w)]^{-1}Q(w).$$

The properties (7)–(8) then imply (10); hence the control law defined by (12) belongs to  $C_3(\Sigma)$ .

c) Finally, let us show that each element of  $C_3(\Sigma)$  can be realized as an element of  $C_1(\Sigma)$ . Given any proper  $K(w)$ , let

$$K(w) = D_0 + wC_0(I - wA_0)^{-1}B_0$$

for some realization  $(A_0, B_0, C_0, D_0)$ . Then

$$(13) \quad \begin{aligned} F_{11} &= 0 & F_{12} &= C_0 & G_1 &= D_0 \\ F_{21} &= 0 & F_{22} &= A_0 & G_2 &= B_0 \end{aligned}$$

defines a control law of the form (3). Moreover,  $I - F_{11}D$  is the identity. Hence the control law (13) belongs to  $C_1(\Sigma)$ .  $\square$

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